#### 恒星進化論 (Stellar Evolution Theory) 梅田 秀之

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講義用 Zoom URL(使うときは): https://u-tokyo-acjp.zoom.us/j/86808825013?pwd=eOwA 1eTsTTdw3quqcrYvUPRen9F6Tb.1











# Supernova explosion simulation (Core collapse SN) t = 8.0e-01 s



### 恒星の進化論

- ・星は誕生から様々に姿を変え、
   宇宙に元素をばらまいていく
- この講義では、これら星の進化 にまつわる現象を紹介し、それを 理解するために基礎となる物理 や、実際に計算を行うための手 法(数値計算法を含む)を解説す る
- また研究の最前線や現在問題となっている事柄も紹介する

#### 前半の重点項目

- ・ 恒星進化の基礎方程式
- 星のポリトロープモデル
- 対流発生の条件
- ・ 恒星はなぜ赤色(超)巨星になるのか
- ・ 混合距離(ミキシング・レングス)理論

## 星の進化論の基礎 (Basic of Stellar Evolution Theory)

#### 星の進化計算

- ・1次元球対称の星の準静的進化
- 基本となる方程式:
  - 連続の式
  - 静水圧平衡の式
  - 状態方程式 P(ρ、T)
  - エネルギー伝播の式
    - ・放射、及び対流
  - エネルギー生成と化学進化
    - ・核反応ネットワーク
  - エネルギー保存の式
  - Opacity

#### 大質量星

- ニュートリノによるエネルギー損失
- 質量放出(Mass Loss)





**太陽の平均密度、温度** 星の平均密度  $< \rho \gg \frac{M}{4\pi_R^3} (= 1.4g/cm^3 \pm 0.4g/cm^3 \pm 0.4g/cm$ 



Polytrope & White dwarfs  $K = c_1 A^{-2} G \rho_c^{\frac{n-1}{n}}$  (KH19.9),  $c_i$ : non dimensional constants  $\& \rho_c \propto \overline{\rho} \propto M R^{-3} = M \left(\frac{A}{z_n}\right)^3$   $\rightarrow A = c_2 \rho_c^{1/3} M^{-1/3}$   $\rightarrow K = c_3 M^{2/3} G \rho_c^{1-\frac{1}{n}-\frac{2}{3}} = c_3 M^{2/3} G \rho_c^{\frac{1}{3}-\frac{1}{n}}$ , also:  $P_c = K \rho_c^{1+\frac{1}{n}} = c_3 G M^{2/3} G \rho_c^{\frac{4}{3}}$   $P_c = 0.48 \ G M^{2/3} G \rho_c^{\frac{4}{3}}$   $(n = \frac{3}{2})$  (1.21)  $= 0.36 \ G M^{2/3} G \rho_c^{\frac{4}{3}}$  (n = 3) (1.22)

Lane-Emden 方程式  
重力ボテンシャルΦを導入:
$$\frac{d\Phi}{dr} = \frac{Gm}{r^2}$$
  
(1.2)  $\rightarrow \frac{dP}{dr} = -\frac{d\Phi}{dr}\rho$  (A)  
Poisson s方程式  
 $\frac{1}{r^2}\frac{d}{dr}(r^2\frac{d\Phi}{dr}) = 4\pi G\rho$  (B)  
(A)  $\rightarrow \frac{d\Phi}{dr} = -\gamma K \rho^{\gamma-2} \frac{d\rho}{dr}$  (P=K $\rho^{\gamma} = K \rho^{1+\frac{1}{n}}$ )  
If  $\gamma \neq 1 \rightarrow \rho = \left(\frac{-\Phi}{(n+1) K}\right)^n$   
(B)  $\rightarrow \frac{d^2\Phi}{dr^2} + \frac{2}{r}\frac{d\Phi}{dr} = 4\pi G \left(\frac{-\Phi}{(n+1) K}\right)^n$   
ここで  $z = Ar$ ,  
 $A^2 = \frac{4\pi G}{(n+1)^n K^n} (-\Phi_c)^{n-1} = \frac{4\pi G}{(n+1) K} (\rho_c)^{\frac{n}{n}}$   
 $w = \frac{\Phi}{\Phi_c} = \left(\frac{\rho}{\rho_c}\right)^{\frac{1}{n}}$  (添え字cは星の中心での値)  
(中心r=0でz=0, \Phi = \Phi\_c, \rho = \rho\_c, w=1)  
とすると、 Lane-Emden方程式が得られる。  
 $\frac{d^2w}{dr^2} + \frac{2}{z}\frac{dw}{dz} + w^n = 0$  or  $\frac{1}{z^2}\frac{d}{dz} \left(z^2\frac{dw}{dz}\right) + w^n = 0$ 

1	$d\left( \int_{-2}^{2} dw \right)$	n	0
$\overline{z^2}$	$\overline{dz} \begin{pmatrix} z & \overline{dz} \\ \overline{dz} & \overline{dz} \end{pmatrix}$	+w =	0
M :	$=4\pi\rho_c R^3$	$\left(-\frac{1}{z}\frac{dw}{dz}\right)$	)
	(		$z=z_n$
_		. \	
$\overline{\rho}$	$=\left(-\frac{3}{4}\frac{dw}{dw}\right)$	/	
$rac{\overline{ ho}}{ ho_c}$	$=\left(-\frac{3}{z}\frac{dw}{dz}\right)$	$\left(\frac{y}{z}\right)_{z=z_n}$	
$\frac{\overline{ ho}}{ ho_c}$	$=\left(-\frac{3}{z}\frac{dw}{dz}\right)$	$\left(\frac{1}{z}\right)_{z=z_n}$	
$\frac{\overline{\rho}}{\rho_c}$	$= \left(-\frac{3}{z}\frac{dw}{dz}\right)$	$\frac{2}{\left(-z^2 \frac{dw}{dz}\right)_{z=z_n}}$	n. Qc/ē
$\frac{\overline{\rho}}{\rho_c}$	$= \left(-\frac{3}{z}\frac{dw}{dz}\right)$	$\frac{2}{z=z_n}$ $\frac{\left(-z^2\frac{dw}{dz}\right)_{z=z}}{4.8988}$	n ec/ē 1.0000
$\frac{\overline{\rho}}{\rho_c}$	$= \left(-\frac{3}{z}\frac{dw}{dz}\right)$	$\frac{2}{\left(-z^2 \frac{dw}{dz}\right)_{z=z_n}}$ $\frac{\left(-z^2 \frac{dw}{dz}\right)_{z=z}}{4.8988}$ 3.14159	n ec/ē 1.0000 3.2898
$\frac{\overline{\rho}}{\rho_c}$	$= \left(-\frac{3}{z}\frac{dw}{dz}\right)$ $\frac{z_n}{\frac{2.4494}{3.14159}}{\frac{3.65375}{3.65375}}$	$\frac{2}{z=z_n}$ $\frac{\left(-z^2 \frac{dw}{dz}\right)_{z=z}}{4.8988}$ $\frac{3.14159}{2.71406}$	n ec/ē 1.0000 3.2895 5.9907
$\frac{\overline{\rho}}{\rho_c}$	$= \left( -\frac{3}{z} \frac{dw}{dz} \right)^{\frac{z_n}{3.65375}}$	$\frac{2}{z=z_n} = z_n$ $\frac{\left(-z^2 \frac{dw}{dz}\right)_{z=z}}{4.8988}$ 3.14159 3.14159 2.71406 2.41105	n εc/ē 1.0000 3.2896 5.9907 11.4025
$\frac{\overline{\rho}}{\rho_c}$	$= \left(-\frac{3}{z}\frac{dw}{dz}\right)^{\frac{2}{3}}$	$\frac{2}{z=z_n}$ $\frac{\left(-z^2 \frac{dw}{dz}\right)_{z=z}}{4.8988}$ $\frac{3.14159}{2.71406}$ $2.71406$ $2.01824$	n 1.0000 3.2898 5.990 11.402 <sup>2</sup> 54.182 <sup>2</sup>
$\frac{\overline{\rho}}{\rho_c}$	$= \left(-\frac{3}{z}\frac{dw}{dz}\right)^{\frac{z_n}{2}}$	$\frac{2}{z=z_n}$ $\frac{\left(-z^2 \frac{dw}{dz}\right)_{z=z}}{4.8988}$ 3.14159 2.71406 2.41105 2.01824 1.79723	n 1.0000 3.2898 5.9907 11.4022 54.1825 622.408
$\frac{\overline{\rho}}{\rho_c}$	$= \left(-\frac{3}{z}\frac{dw}{dz}\right)^{\frac{z_n}{2}}$	$\frac{2}{z=z_n}$ $\frac{\left(-z^2 \frac{dw}{dz}\right)_{z=z}}{4.8988}$ $\frac{3.14159}{2.71406}$ $\frac{2.41105}{2.01824}$ $\frac{1.79723}{1.73780}$	n ec/ē 1.0000 3.2896 5.9907 11.4025 54.1825 622.408 6189.47







準静的収縮 Quasi-static Contraction
$E_{GR} = -\int_{0}^{R} \frac{Gm\rho}{r} 4\pi r^{2} dr = -\frac{3GM^{2}}{5R} \qquad (\rho = -\Xi \mathcal{O}) = 0$
一党スに $E_{GR} \approx -\frac{GM^2}{R}$
$(1.5) \rightarrow P_c \propto < P > \approx \frac{GM^2}{4\pi R^4} \qquad (1.8)$
$ \rho_c$ は星の平均密度に比例 $ \rho_c \propto \frac{M}{\frac{4}{3}\pi R^3} $
$\frac{P_c}{\rho_c} \propto \frac{GM}{R}$ (1.9), $\frac{P_c^3}{\rho_c^4} \propto G^3 M^2$ (1.10)
理想気体状態方程式 $P_c = \frac{k}{\mu m_u} \rho_c T_c$
$+(1.10) \rightarrow \frac{T_c^3}{\rho_c} \propto G^3 M^2$ (1.11)
(1.11)式 ⇒ $M$ 一定のとき $\rho_c \propto T_c^3$











nyarogen barning
<ul> <li>(1.14)→ M &lt; 0.08M<sub>☉</sub> - T<sub>max</sub> &lt;~ 10<sup>7</sup> K Hydrogen can't be ignited.</li> <li>→ Brown dwarfs (褐色矮星, supported by the degenerate pressure)</li> </ul>
• $T \sim 1.5 \times 10^7 \text{ K}$ : pp (proton-proton) chain
$\begin{array}{l} p+p \to d+e^{+}+\nu_{e} \\ p+d \to {}^{3}\text{He}+\gamma \\ 1) {}^{3}\text{He}+{}^{3}\text{He} \to {}^{4}\text{He}+p+p \ (pp1) \\ 2) {}^{3}\text{He}+{}^{4}\text{He} \to {}^{7}\text{Be}+\gamma \\ 2a) e^{-}{}^{7}\text{Be} \to {}^{7}\text{Li}+\nu_{e} \\ p{}^{+7}\text{Li} \to {}^{4}\text{He}+{}^{4}\text{He} \ (pp2) \\ 2b) p{}^{+7}\text{Be} \to {}^{8}\text{B}+\gamma \\ {}^{8}\text{B} \to {}^{8}\text{Be}^{*}+e^{+}+\nu_{e} \\ {}^{8}\text{Be}^{*} \to {}^{4}\text{He}+{}^{4}\text{He} \ (pp3) \\ \epsilon_{pp} \sim 2.36 \times 10^{6} \ X_{H}^{2}\rho \ T_{6}^{-2/3} \\ \varkappa exp(-33.8 \ T_{6}^{-1/3}) \ erg \ g^{-1}sec^{-1} \end{array}$





















光球

彩層



エネルギー保存の式 (KH30)
<ul> <li>完全に静的(stationary)な場合,エ ネルギー生成率を持つ厚さdrの 球殻を通過するときのenergy flow rate (luminosity)の変化量は</li> </ul>
dL=4πr <sup>2</sup> ρεdr=εdm 又は
• 一般に
$dq = \left(\varepsilon - \frac{\partial L}{\partial m}\right) dt = T ds \rightarrow T \frac{\partial s}{\partial t} = \varepsilon - \frac{\partial L}{\partial m}$
$\varepsilon = \varepsilon_n - \varepsilon_v,  \varepsilon_g \equiv -T \frac{\partial s}{\partial t}  \succeq \Rightarrow \Im \succeq$
$\mathcal{E}_n$ : nuclear energy generation rate
$\mathcal{E}_{v}$ : neutrino energy loss rate
$\frac{\partial L}{\partial m} = \varepsilon_n - \varepsilon_v + \varepsilon_g$
(1.17:エネルギー保存の式)

Energy conservation
Modifying $\mathcal{E}_g$ into a more convenient form
(using the first law of thermodynamics)
$Tds = du + Pdv = \left(\frac{\partial u}{\partial T}\right)_{v} dT + \left[P + \left(\frac{\partial u}{\partial v}\right)_{T}\right] dv$
$= c_v dT - \frac{P\delta}{\rho^2 \alpha} d\rho  (v = 1/\rho : \text{specific volume},$
$c_v$ : specific heat at constant volume)
$\alpha \equiv \left(\frac{\partial \ln \rho}{\partial \ln P}\right)_T, \ \delta \equiv -\left(\frac{\partial \ln \rho}{\partial \ln T}\right)_P$
$\varepsilon_{g} = -T\left(\frac{\partial s}{\partial t}\right) = -c_{v}\frac{\partial T}{\partial t} + \frac{P\delta}{\rho^{2}\alpha}\frac{\partial\rho}{\partial t}$
$= -c_p T \left( \frac{1}{T} \frac{\partial T}{\partial t} - \frac{\nabla_{ad}}{P} \frac{\partial P}{\partial t} \right)  (1.18)$
$c_p$ : specific heat at constant pressure
$\nabla_{ad} \equiv \left(\frac{\partial \ln T}{\partial \ln P}\right)_s = \frac{P\delta}{T\rho \ c_p}$
: adiabatic temperature gradient (1.19)

## 星の進化計算 Full set of equations ・ Rewrite equations as a function of m



$$\frac{\partial m}{\partial m} = 4\pi r^4 - 4\pi r^2 - \partial t^2 \quad \text{(with acceleration term)}$$

$$\frac{\partial \mathbf{L}}{\partial m} = \varepsilon_n - \varepsilon_\nu - c_P \quad \frac{\partial T}{\partial t} + \frac{\delta}{\varrho} \quad \frac{\partial P}{\partial t}$$

$$\frac{\partial T}{\partial m} = -\frac{GmT}{4\pi r^4 P} \nabla \quad \text{,} \quad (\nabla = \nabla_{rad} = \frac{3\kappa LP}{16\pi acT^4 Gm}, \nabla = \nabla_{convec})$$

$$\frac{\partial Y}{\partial t} = m \cdot \left( \sum_{i=1}^{N} \frac{\partial F}{\partial t} \right)$$

$$\frac{\partial X_i}{\partial t} = \frac{m_i}{\varrho} \left( \sum_j r_{ji} - \sum_k r_{ik} \right) \quad ($$
 境界条件 KH p.93~)   
↓

- Usually solved by the Henyey method
   Non-liner boundary condition problem (boundary conditions depend on time implicitly)
- Define  $\delta y$  as the difference between the temporal and true solution. Then linearize the equation for  $\delta y$  to solve
- Repeat (iterate) this procedure until  $\delta {\bm y}$  becomes sufficiently small





